

# Quantitative geomorphology of the White Mountains (California) using detrital apatite fission track thermochronology

### Pieter Vermeesch<sup>1</sup>

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[1] Detrital thermochronology has been proposed as a method for measuring average basin-wide erosion rates. This paper illustrates how to use detrital apatite fission track (AFT) thermochronology to map out where in a basin erosion takes place. Five samples of detrital AFT ages were collected on an alluvial fan that is fed by the Marble Creek drainage basin in the northern White Mountains (California). Using a digital elevation model (DEM) to characterize the basin hypsometry and a few published basement samples to constrain the age-elevation curve of the catchment, the detrital AFT distribution was predicted. Comparing the observed with the predicted age distributions reveals that localized rockfall events provide the sediment source of the currently active Marble Creek, but a composite sample from the entire alluvial fan indicates that, over longer time scales, the entire catchment contributes material to the debris-flow dominated fan, with more material being derived from lower elevations than from higher up the Marble Creek Canyon. The observed AFT age distribution is compared with the hypsometric predictions using the "Cumulative Age Distribution" (CAD) which is the cumulative distribution of the measured ages. In contrast with probability density estimators and their cumulative equivalents, the CAD requires no numerical smoothing while properly accounting for (unequal) measurement uncertainties.

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### 1. Introduction

[2] Radiometric cooling ages ( $^{40}$ Ar/ $^{39}$ Ar, fission track, (U-Th)/He) of exhumed fault blocks generally increase with elevation. For catchments draining such terranes, it is possible to predict detrital age distributions if the relationship between age and elevation is either assumed or known, if the catchment hypsometry is known, and under some additional assumptions, which are discussed below.

[3] A few studies have explored this for the  ${}^{40}\text{Ar}/{}^{39}\text{Ar}$  system. If erosion is in a steady state over geologic time, then  ${}^{40}\text{Ar}/{}^{39}\text{Ar}$  cooling ages are expected to decrease linearly with depth, or increase linearly with elevation. In a theoretical study, *Stock and Montgomery* [1996] argue that, under the assumption of a thermal gradient, the range of detrital cooling ages can be used to estimate (paleo-)relief. Going one step further, *Brewer et al.* [2003] proposed a method to estimate average basin-wide erosion rates by matching the shape of detrital age distributions with the area-elevation curve (="hypsometry") of the catchment. In a recent paper, *Ruhl and Hodges* [2005] introduced a hybrid approach using an extensive data set of 692 detrital muscovite  ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ 

wide erosion rates were estimated from the range of detrital cooling ages, while the shape of the detrital age distributions was used to test the validity of several assumptions made by Stock and Montgomery and Brewer et al.: (1) the assumption of steady state erosion and topography, which is required for a predictable (typically linear) age-elevation curve, and (2) the assumptions of uniform modern erosion rates, negligible sediment storage in the catchment, and adequate mixing of the sediments, which are necessary for the convolution of this age-elevation curve with the catchment hypsometry, but may be invalidated by inhomogeneous lithologies, structural geology or the presence or absence of vegetation.

[4] If these assumptions hold, Ruhl and Hodges [2005] argue, then the hypsometric curve must match the observed detrital age distribution. Strictly speaking, this does not mean that all assumptions hold if and only if the hypsometry matches the measured detrital age distribution. More importantly, if the measured age distribution does not match the hypsometry, it is difficult to assess which of the assumptions were violated and to what extent. In only one of Ruhl and Hodges' four catchments did the measured match the predicted age distribution, indicating that steady state erosion might exist. For the other three catchments, it is unclear whether this means that erosion and topography are not in steady state, erosion rates are not uniform or sediments are not well mixed. Is one problem responsible for all catchments or are different assumptions violated in different catchments? For each of the previous studies, the age-elevation relationship was unknown. If known, would

<sup>&</sup>lt;sup>1</sup>Institute of Isotope Geology and Mineral Resources, ETH Zürich, Zürich, Switzerland.

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**Figure 1.** (a) AFT data of *Stockli et al.* [2000] reveal an exhumed Partial Annealing Zone (PAZ). Each paleodepth under a Miocene erosional unconformity corresponds to a unique AFT age. The lower part of this curve is exposed on the western side of the range (box labeled "W"), whereas the upper part is exposed on the eastern side (box labeled "E"). (b) For each location on the northern White Mountains, the paleodepth was calculated, and using (a), the corresponding AFT age was computed, and color-coded. The yellow polygon outlines the Marble Creek drainage basin.

that have explained the mismatches that resulted from assuming a linear age-elevation relation? The present paper avoids many of these questions in a carefully selected field area, where assumption (1) is not necessary, enabling a semi-quantitative assessment of assumption (2). The following sections will outline a method to map out the erosion rate distribution in a watershed by looking at the frequency distribution of detrital fission track cooling ages in apatite crystals derived from it. This idea was independently developed and published by Stock et al. [2006], who studied detrital (U-Th)/He ages from two catchments in the eastern Sierra Nevada, on the opposite side of the Owens Valley. Although the basic idea behind the work of Stock et al. is identical to the present study, there are important methodological differences in the way the data are interpreted (section 2).

[5] The method is illustrated in the context of a simple drainage basin in the White Mountains, an eastward-tilted fault block on the California-Nevada border. The S-N trending White Mountains fault block is bounded on the west by the White Mountains fault zone, which is dated at 12 Ma by apatite fission track (AFT) and (U-Th)/He dating at different structural levels on the fault block [Stockli et al., 2000, 2003]. A mid-Miocene erosional unconformity found on the eastern flank of the northern White Mountains is tilted  $\sim 25^{\circ}$  to the east [Stockli et al., 2000, 2003]. Linearly extrapolating this Miocene paleo-surface would imply up to 8 km of normal displacement along the White Mountains fault zone. The eastern boundary of the White Mountains is marked by the dextral Fish Lake fault zone, which initiated at 6 Ma, and corresponds to the onset of strike-slip motion on the Walker Lane Belt [Stewart, 1988; Reheis and Dixon, 1996; Reheis and Sawyer, 1997]. At 3 Ma, the White Mountains fault zone was reactivated in an oblique rightlateral strike-slip sense, marking the progression of Walker Lane tectonism from east to west [Stockli et al., 2003]. The dip-slip component of motion was large enough that its

signal can be recognized in the exhumed (U-Th)/He Partial Retention Zone (PRZ) of the northern White Mountains [*Stockli et al.*, 2000, 2003].

[6] Stockli et al. [2000] measured AFT and apatite (U-Th)/ He ages along a transect in the northern White Mountains (Figures 1 and 2), revealing an exhumed fission track Partial Annealing Zone (PAZ, Figure 1a). Defining "paleodepth" as the perpendicular distance to the assumed tilted mid-Miocene erosional surface, each paleodepth in Figure 1a corresponds to a unique AFT age and conversely, each AFT age corresponds to a unique paleodepth. AFT ages can be predicted by computing the paleodepth for each pixel of a digital elevation model (DEM), and assigning the corresponding AFT age to it. This is exactly how Figure 1b was generated. The paleodepth values of [Stockli et al., 2000, 2003] are based on the interpretation that a bedding dip in the eastern White Mountains could be reliably projected across the range into space (Figure 1b). It is, however, possible that this surface was folded, potentially causing significant uncertainties on the paleodepths. This would have little or no effect on the reconstructed AFT age-distribution. Paleodepth is just used as an intermediate step between AFT age and topography. Exactly via which numerical paleodepth-value an AFT age is mapped to a topographic location is irrelevant, as long as the mapping is correct.

[7] If we assume that the sand grains were uniformly derived from the entire drainage [*Ruhl and Hodges*, 2005, assumption (2)], it is possible to predict the detrital AFT grain-age distribution. Detrital thermochronological data are usually represented by estimates of their probability density, whose interpretation often involves deconvolution into Gaussian subpopulations [*Galbraith and Green*, 1990; *Brandon*, 1996]. Cumulative distributions are an alternative to probability density estimates that have recently gained considerable popularity [*Brewer et al*, 2003; *Amidon et al.*, 2005; *Ruhl and Hodges*, 2005; *Hodges et al.*, 2005]. This



**Figure 2.** Landsat image of the Marble Creek drainage basin and its alluvial fan, with indication of the sample locations and the underlying geology, modified from the works of *Saucedo et al.* [2000] and *McKee and Conrad* [1996].

paper introduces a new kind of cumulative distribution which is slightly different from these previous studies. The reasons why this so-called "Cumulative Age Distribution" is preferred to probability density estimates and previous cumulative probability curves are discussed in the following section.

### 2. Probability Density Function (PDF) vs. Cumulative Synoptic Probability Density Function (CSPDF) vs. Cumulative Age Distribution (CAD)

[8] Detrital thermochronological age distributions can be visualized either by probability density estimates or by cumulative probability plots. For the latter, two different kinds of cumulative probability diagrams will be discussed. The various acronyms used in the literature are summarized in Table 1. This section is an attempt to shed a little light in this rather confusing myriad of statistical tools. Each of the options will be defined and compared with its alternatives. After this section, only the terms "observed CAD" and "predicted CAD" will be used. Readers who are just

interested in the applications part of this paper can skip to section 3.

### 2.1. Probability Density Function (PDF)

[9] The information relevant to the kind of detrital thermochronology discussed in this paper is not so much the actual ages, but their probability distribution. Underlying any set of detrital ages is a Probability Density Function (PDF), describing the probability of occurrence of any detrital age *t*:

$$Pr(a < t < b) = \int_{a}^{b} pdf(t)dt \qquad \forall a < b$$
(1)

[10] In practice, the PDF can never be precisely known because that would require an exhaustive sampling of the detrital population. Therefore we must work with estimates of the PDF based on a finite sample of detrital ages (typically tens to hundreds of ages). Besides limited data, measurement uncertainty is a second factor reducing the precision of density estimates. The most popular estimators of probability density are histograms and "kernel density

Term	Definition
PDF	Probability Density Function
CDF	Cumulative Density Function
SPDF, CSPDF	Synoptic Probability Density Function and Cumulative Synoptic Probability Density Function, respectively
SPDF <sub>z</sub>	Hypsometry, i.e., the probability (or area) of any given elevation within a catchment
SPDF <sub>t</sub>	This curve is obtained from $n$ age measurements by: (1) assigning a Gaussian distribution to each age measurement with standard deviation equal to the measurement uncertainty; (2) "stacking" all these Gaussian distributions; and (3) normalizing the area under the resulting curve
$CSPDF_{z}, CSPDF_{t}$	Cumulative versions of SPDF, and SPDF, respectively
SPDF <sub>z*</sub> , SPDF <sub>t*</sub> , CSPDF <sub>z*</sub> , and CSPDF <sub>t*</sub>	In the nomenclature of <i>Ruhl and Hodges</i> [2005], $z^*$ and $t^*$ are the normalized versions of $z$ and $t$ , respectively, i.e., $z^* = z/(\max(z) - \min(z))$ and $t^* = t/(\max(t) - \min(t))$ . Thanks to the normalization, elevations and ages can be directly compared with each other. In this paper, the asterisks are dropped and it is clear from the context whether the normalized or the raw variables are used.
CSPDF <sub><i>i</i>*m</sub>	A "model CSPDF <sub>t</sub> curve". If <i>n</i> measurements were used to calculate SPDF <sub>t</sub> , then CSPDF <sub>t</sub> is calculated by randomly selecting <i>n</i> points from SPDF <sub>z</sub> . First, a nominal normally distributed "analytical uncertainty" like that of the actual grain ages is associated with each of the <i>n</i> elevations, the Gaussian distributions are summed, and the resulting curve is normalized to form a CSPDF <sub>t</sub> curve
(Observed) CAD	"Cumulative Age Distribution," a discrete step-function with the sorted detrital age measurements on the $x$ axis and their respective ranks on the $y$ axis
Predicted CAD	Is calculated by randomly selecting a large number (for example, $k = 1000$ ) of points from SPDF <sub>z</sub> , and assigning a synthetic "measurement error" to each of them by adding a random number from the error distribution of one of the n measurement uncertainties of the "real" measurements which were used for the construction of SPDF <sub>t</sub> and CSPDF <sub>t</sub> . The k "synthetic measurements" are then sorted and plotted as a CAD, i.e., a discrete step-function with the sorted measurements on the x axis and their respective ranks on the y axis. Thus, the predicted CAD is practically identical to the CSPDF <sub>t</sub> <sub>m</sub> .

Table 1. Definition of Acronyms Used in the Literature and in This Paper

plots" [e.g., *Silverman*, 1986]. Both of these methods apply some degree of "smoothing" to the data, either by binning them into a histogram, or by assigning a Gaussian uncertainty distribution to each measurement:

$$\widehat{\text{pdf}}(t) = \frac{1}{n} \sum_{i=1}^{n} N(t|\mu = t_i, \quad \sigma = \alpha \hat{\sigma}(t_i))$$
(2)

where  $N(t|\mu, \sigma)$  is the normal distribution of t with mean  $\mu$  and standard deviation  $\sigma$ , and  $t_i$  and  $\hat{\sigma}(t_i)$  are the measured ages and their respective  $1\sigma$  uncertainties. To illustrate the different approaches to detrital thermochronological density estimation, consider the degenerate case of a "diving board" hypsometry: all detrital grains are derived from a single elevation, corresponding to a single "true" age  $t_{\text{true}}$ . The PDF of the true ages is a delta function (spike at  $t_{\text{true}}$ , zero probability elsewhere). For further simplification, all grains have identical, Gaussian measurement uncertainties. In the following,  $t_{\text{true}} = 10$  Ma so all grains are 10 Ma old and have Gaussian measurement uncertainties of 1 Ma.

[11] Suppose we have access to an infinite number of measurement from this detrital population. The PDF of these age *measurements* can then be determined by a histogram with infinitesimal binwidth or a kernel density estimate with infinitesimal  $\alpha$ . Note that the PDF of the measurements is not the same as the PDF of the underlying *ages* (Figure 3a). Unless we deconvolve the measurement uncertainties, the measurement distribution will always be a "smoothed" version of the "true" age distribution. In our toy example, the *age distribution* is a delta-function at 10 Ma, whereas the *measurement distribution* is a Gaussian distribution with mean 10 Ma and standard deviation 1 Ma (Figure 3a).

[12] Given a set of age data, the Gaussian kernel density estimator stacks a bell curve on top of each measurement (equation (2) and Figure 3b). Repeating this for a large number of measurements drawn from our "diving board" hypsometry yields a Gaussian distribution with mean 10 Ma and standard deviation  $\sigma = \sqrt{(1 \text{ Ma})^2 + (\alpha \times 1 \text{ Ma})^2}$ . Thus,  $\widehat{pdf}$  is "double-smoothed": once by the measurement uncertainties, and a second time by the construction of the kernel density estimator. The amount of additional smoothing depends on the parameter  $\alpha$ . Although it can be shown that  $\alpha = 0.6$  is an optimal value [Silverman, 1986; Brandon, 1996], previous studies by Brewer et al. [2003], Ruhl and *Hodges* [2005] and *Stock et al.* [2006] have used  $\alpha = 1$ , and so does Figure 3b. Ruhl and Hodges gave this curve the name "Synoptic Probability Density Function" (SPDF). These authors distinguish between three kinds of SPDF.  $SPDF_z$  is the true underlying age distribution, in the hypothetical case of errorless measurements (dashed lines in Figure 3). In our toy example,  $SPDF_z$  is a delta function.  $SPDF_t$  is the kernel density estimator generated by equation (2) (gray lines in Figure 3). Finally,  $SPDF_{t*m}$  effectively is the PDF of the measurements (black lines in Figure 3). Because  $SPDF_{t*m}$  is only smoothed once, whereas  $SPDF_t$  is smoothed twice, SPDF<sub>t</sub> is a biased estimator of SPDF<sub>t\*m</sub> (Figure 3c).

[13] One of the requirements for the application of Gaussian kernel density estimation is that the measurement uncertainties are normally distributed. This may be a reasonable assumption for  ${}^{40}$ Ar/ ${}^{39}$ Ar thermochronology, but not necessarily for fission tracks, which are governed by a Poisson process. However, by using the logistic transform, a set of fission track data can be recast in terms of a new parameter *z* [*Brandon*, 1996], which is estimated by

$$\hat{z} = \ln(\lambda \zeta \ g\rho_{\rm D}) + \ln\left(\frac{N_{\rm s} + 0.5}{N_{\rm i} + 0.5}\right) \tag{3}$$

where  $\lambda$  is the decay constant of <sup>238</sup>U (=1.55125 × 10<sup>-10</sup> a<sup>-1</sup>),  $\zeta$  (zeta) is the calibration factor measured on

an AFT age standard, g is the geometric factor (=0.5),  $N_s$  is the number of spontaneous fission tracks,  $N_i$  is the number of induced tracks in a mica detector, and  $\rho_D$  is the induced track density of a glass standard that was irradiated along with the



sample.  $N_{\rm s}$  and  $N_{\rm i}$  are Poisson variables, but  $\hat{z}$  is normally distributed with a standard error

$$\hat{\sigma}(z) = \sqrt{\frac{1}{N_{\rm s} + 0.5} + \frac{1}{N_{\rm i} + 0.5}} \tag{4}$$

# 2.2. Cumulative Synoptic Probability Density Function (CSPDF)

[14] The probability density function (PDF) is intimately linked to the cumulative density function (CDF). The relationship between PDF and CDF is:

$$\operatorname{cdf}(t) = \int_{-\infty}^{t} \operatorname{pdf}(x) \mathrm{d}x$$
 (5)

$$pdf(t) = \frac{d(cdf(t))}{dt}$$
(6)

[15] PDF and CDF are standard statistical terms. In the nomenclature of Ruhl and Hodges [2005], the specific case of a Gaussian kernel density estimator with  $\alpha = 1$  is named SPDF, and the corresponding CDF is named the Cumulative Synoptic Probability Density Function (CSPDF). Thus, the CSPDF is defined by using SPDF instead of PDF in equation (5). Although SPDF and CSPDF are interchangeable from a statistical point of view, the CSPDF has recently gained considerable popularity for two reasons. First, the cumulative distribution has intuitive significance, as its shape mimics the shape of the cumulative hypsometry (modulated by the age-elevation curve). A second advantage of cumulative plots is the ease of comparing different data sets by using the Kolmogorov-Smirnov (K-S) goodness-of-fit test. The K-S test determines if the maximum vertical distance between two cumulative distributions can be explained by random sampling effects alone. As illustrated by Amidon et al. [2005], using the CSPDF in combination with the K-S test is a useful tool for comparing two detrital data sets. However, we will next see that the CSPDF should not be used for the purpose of comparing a detrital age distribution with hypsometric predictions.

[16] Revisiting the toy example of a "diving board" hypsometry, the CDF of the true ages is a step-function at  $t_{\text{true}} = 10$  Ma (Figure 4). The theoretical CDF of the measured ages ( $\approx$ CSPDF $_{t^*m}$  curve of *Ruhl and Hodges* [2005]) is the cumulative normal distribution with a mean of 10 Ma and standard deviation of 1 Ma (red curve on

**Figure 3.** (a) Dashed line: expected (errorless) age distribution of a "diving board" hypsometry, black line: measurement distribution including 1 Ma (normally distributed) measurement uncertainty; (b) circles are three measurements drawn from the measurement distribution. Using the nomenclature of *Ruhl and Hodges* [2005], SPDF<sub>z</sub> is the hypsometric curve and SPDF<sub>t</sub> is the Gaussian kernel density estimator of the measured age distribution; (c) as the number of measurements increases (50 in this figure), SPDF<sub>t</sub> converges to a normal distribution with standard deviation  $\sigma = \sqrt{2}$ . SPDF<sub>t\*m</sub> is a normal distribution with standard deviation  $\sigma = 1$ .



**Figure 4.** The cumulative equivalent of Figure 3c. The dashed step-function is the cumulative hypsometry (CSPDF<sub>z</sub>), corresponding to the "true age distribution," which could only be measured if we had access to errorless measurements. Gray circles are measurements, black circles are the Cumulative Age Distribution (CAD). The black curve is CSPDF<sub>t\*m</sub>, which coincides with the theoretical "predicted CAD" obtained from an infinite number of synthetic measurements including measurement uncertainties. The observed CAD is an unbiased estimator of the predicted CAD. The gray curve is CSPDF<sub>t</sub> calculated from the 50 measurements and their respective uncertainties. CSPDF<sub>t</sub> is not a good estimator of CSPDF<sub>t\*m</sub>.

Figure 4). In contrast, the cumulative kernel density estimator CSPDF<sub>t</sub> (gray curve on Figure 4) is the cumulative normal distribution with a mean of 10 Ma and standard deviation of  $\sqrt{2}$  Ma. Thus, CSPDF<sub>t</sub> is not a good estimator of CSPDF<sub>t\*m</sub>, for the same reason why SPDF<sub>t</sub> is not a good estimator of SPDF<sub>t\*m</sub> (Figure 3). In other words, the CSPDF is not a good tool for comparing detrital data sets with hypsometric predictions, which is exactly the goal of this paper. Fortunately, the misfit caused by the "double smoothing" of CSPDF<sub>t</sub> does not greatly affect the conclusions of *Ruhl and Hodges* [2005] and *Stock et al.* [2006], because the analytical uncertainties of their <sup>40</sup>Ar/<sup>39</sup>Ar and (U-Th)/He data are relatively small. The situation would be worse for the less precise AFT data presented here.

[17] The CSPDF method can be "fixed" by smoothing the CSPDF<sub>*t*\*m</sub> a second time. In practice, CSPDF<sub>*t*\*m</sub> can be constructed by collecting a large number of synthetic "measurements" from the hypsometry and adding a synthetic measurement error to them. The second smoothing step would then involve stacking a bell curve on top of each of the synthetic measurements, as in equation (2). Instead of this cumbersome "fix," the Cumulative Age Distribution (CAD) is introduced as a simpler alternative to the CSPDF method.

#### **2.3.** Cumulative Age Distribution (CAD)

[18] One of the most significant advantages of using cumulative distributions instead of probability density esti-

mates is not exploited by the CSPDF. Whereas it is impossible to visualize probability densities without using at least some degree of smoothing (either by binning or by stacking Gaussian kernels), this is not the case for cumulative distributions. The Cumulative Age Distribution (CAD) is a discrete step-function with the sorted detrital age measurements on the *x* axis and their respective ranks on the *y* axis (Figure 4). The (measured or "observed") CAD is an unbiased estimator of *Ruhl and Hodges* <sup>'</sup> [2005] CSPDF<sub>*t*\*m</sub>, which will hereafter be named the "predicted CAD."

[19] At first glance, it seems like the CAD does not properly account for variable measurement uncertainties. The CSPDF explicitly takes into account analytical uncertainties ( $\hat{\sigma}(t_i)$  in equation (2)), by "spreading out" imprecise measurements with wider Gaussian kernels. In contrast with this, the observed CAD gives equal "weight" to all measurements. The observed CAD gets around the need for kernel smoothing by shifting the uncertainty weighting to the predicted CAD. The predicted CAD is computed from the hypsometry by simulating the detrital sampling process. First, a number of synthetic ages are generated from the hypsometry. Then, synthetic measurement errors are added to each of these values, comparable in size to the real analytical uncertainties. From these synthetic measurements, a predicted CAD is calculated in exactly the same way as the observed CAD. Thus, the measurement uncertainties are properly accounted for by the predicted CAD, and there is no need to add them to the observed CAD a second time. Note that the same procedure is also part of the CSPDF method, because the "predicted CAD" is essentially the same as *Ruhl and Hodges* ' [2005] CSPDF<sub>t\*m</sub>.

# 2.4. Taking Into Account Unequal Measurement Uncertainties

[20] In the toy example discussed before, all measurements had equal measurement uncertainties. This is seldom the case in real world applications, particularly when fission track dating is involved. Most importantly, AFT age uncertainties are a sensitive function of the number of spontaneous fission tracks. Young grains have fewer spontaneous tracks than older grains of similar U concentration. This results in widely variable measurement uncertainties ranging from a few percent for old, U-rich grains to more than 100% for U-poor grains containing little or no fission tracks. As explained in the previous section, measurement uncertainties are incorporated in the predicted, rather than the observed CAD. The problem of unequal measurement uncertainties can be mitigated by using Brandon's [1996] logarithmic "z-transformation" (equation (3)). Although this is a valid approach, we will use the regular age-equation in the following.

[21] The sand and gravel samples discussed in this paper were dated with the external detector method [*Hurford and Green*, 1983]. The age equation for this method is:

$$t = \frac{1}{\lambda} \ln \left( 1 + \lambda \zeta g \rho_{\rm D} \frac{N_{\rm s}}{N_{\rm i}} \right) \tag{7}$$

with all variables as in equation (3). Using the external detector method, fission track ages (t) are roughly



**Figure 5.** Samples A and B are large granitic boulders on the alluvial fan. Their AFT age suggests that they were derived from the base of the mountain range. Sledge hammer ( $\sim$ 80 cm) for scale.

proportional to the ratio of the expected number of spontaneous tracks ( $N_s$ ) in the mineral grain to the expected number of tracks induced by neutron irradiation ( $N_i$ ):  $t \propto N_s$ / $N_i$ . However, if  $N_s$  and/or  $N_i$  are small numbers (<10), then the observed ratio of spontaneous ( $\hat{N}_s$ ) to induced ( $\hat{N}_i$ ) tracks can potentially be very different. For example, if  $N_s = 2$ , there is 14% chance that  $\hat{N}_s = 0$ , resulting in an AFT age  $\hat{t} \propto \hat{N}_s / \hat{N}_i = 0$ . Assuming that there is no systematic correlation between  $N_i$  and t, the effect of Poisson-distributed counting statistics on the CAD can be modeled as follows:

[22] 1. Consider a probability distribution of AFT ages, for example, k = 1000 numbers drawn from the cumulative hypsometry.

[23] 2. For each of these ages  $t_j$   $(1 \le j \le k)$ , randomly select a  $N_i$  value  $(N_i^j$ , say) from the database of measurements (Tables S5 and S6 of the Auxiliary material<sup>1</sup>).

[24] 3. Compute the expected number of fission tracks  $(N'_s)$  corresponding to  $t_i$  and  $N'_i$  by rearranging equation (7):

$$N_s^j = \frac{N_i^j}{\lambda \zeta g \rho_{\rm D}} \left( e^{\lambda t_j} - 1 \right) \tag{8}$$

[25] 4. Generate random replicates  $N_s^{j^*}$  of  $N_s^j$  and  $N_i^{j^*}$  of  $N_i^j$  by sampling at random from a Poisson distribution:

$$N_s^{j^*} \sim \operatorname{Poiss}(N_s^j) \quad \text{and} \quad N_i^{j^*} \sim \operatorname{Poiss}(N_i^j)$$
(9)

[26] 5. Plug  $N_{s_{*}}^{j_{*}}$ ,  $\zeta^{j}$  and  $N_{i}^{j_{*}}$  into equation (7). This yields a replicate age  $t_{j}^{*}$ . Doing this for all k errorless AFT ages from the expected CAD yields a new CAD (the "predicted CAD") that does take into account Poisson-distributed measurement uncertainties. Note that this CAD effectively follows the definition of *Ruhl and Hodges*' [2005] CSPDF<sub>t\*m</sub> curve.

### 3. CADs of the Marble Creek Catchment 3.1. Predicted CAD

[27] We now return to the White Mountains. To illustrate the application of detrital thermochronology to quantitative geomorphology, consider granitoid (quartz monzonite) boulders A and B (Figure 5) on the alluvial fan that is fed by the Marble Creek drainage. Large boulders of several meters diameter are a characteristic feature of the alluvial fans of the northern Owens Valley [e.g., *Beaty*, 1963, Figure 16]. They can be found up to several kilometers from the range front and are evidence of the exceptional power of the rare flash floods and debris flows that are responsible for the

<sup>&</sup>lt;sup>1</sup>Auxiliary materials are available at ftp://ftp.agu.org/apend/jf/2006jf000671.



**Figure 6.** Comparison of predicted (line symbols) and observed (point symbols) CADs. The gray band contains 95% of all possible CADs for the granitic part of the catchment, assuming uniform erosion and taking into account Poisson-based measurement uncertainties.

bulk of sediment transport on the Marble Creek alluvial fan [*Beaty*, 1963]. The Marble Creek catchment area is 15.82 km<sup>2</sup>, 14.01 km<sup>2</sup> of which consist of quartz monzonite, with only a small portion of Paleozoic marble (Figure 2). Boulders A and B both have an AFT age of  $10 \pm 2$  Ma, indicating that they were derived from the base of the range (Figure 5). This method is easily extended to samples of many, rather than one clast. Sand sample C was collected at the apex of the alluvial fan (Figure 2). If erosion is assumed to be uniform across the entire Marble Canyon, then we can calculate a predicted age distribution by exhaustively sampling all the pixels of the digital elevation model (Figure 1) and predicting their respective expected AFT cooling ages.

[28] Previous studies [*Stock and Montgomery*, 1996; *Brewer et al.*, 2003; *Ruhl and Hodges*, 2005] assumed that exhumation is laterally continuous and uniform. In this case, the expected detrital age distribution can be calculated by simply convolving the age-elevation curve with the hypsometry. In the case of the White Mountains, however, it is known that the assumption of uniform exhumation does not hold, and that  $\sim 25^{\circ}$  of eastward tilting has taken place since the late Miocene [*Stockli et al.*, 2003]. Therefore paleoisotherms are not horizontal, and the simple hypsometric approach is not valid.

[29] Relatively little material will be derived from the lower elevations or higher paleodepths, because the basin is the narrowest at its mouth (Figure 2). The CAD (Figure 6) serves as a proxy for the age-elevation curve of the basement, defined by Figure 1a. "Steep" parts of the age-elevation curve are defined by elevation intervals over which the AFT ages are approximately constant (Figure 1a). These ages will be over-represented in the grain-age distribution and correspond to steep parts of the CAD. Likewise, relatively flat portions of the age-elevation curve correspond to intervals of the basement over which the AFT ages change rapidly with elevation. These ages will be under-represented in the detrital grain-age distribution and correspond to relatively flat parts of the CAD. Marble Creek sediments only sample ages corresponding to the lower part of the basement age-elevation curve. Older ages can be found in sediments on the eastern side of the mountain range (Figure 1).

[30] The predicted CAD shown in black on Figure 6 assumes zero measurement uncertainties. According this curve, the youngest expected detrital AFT grain-age should be 12 Ma, or 10 Ma taking into account the measurement uncertainties reported by *Stockli et al.* [2000]. However, the observed CAD is not computed from composites of many apatites, as in Stockli et al. and Figure 1a, but on individual AFT grain-ages, which have much larger uncertainties that are governed by a Poisson distribution. Using the database of the measured  $\hat{t}$ ,  $\hat{N}_{\rm s}$  and  $\hat{N}_{\rm i}$  values provided in the Auxiliary material, section 2.4 explained how to compute an equivalent predicted CAD that accounts for these uncertainties (the white curve in Figure 6).

[31] Apart from the measurement uncertainties inherent to the fission track method, additional uncertainty is introduced by the finite sample size, 97-100 apatite grains for this study. This ensures us that the largest population fraction that was not missed with 95% probability is less than 6% of the total [Vermeesch, 2004]. 5000 random replicates of the predicted CAD were generated by repeatedly sampling 97–100 times from the predicted age distribution (white curve of Figure 6), and selecting the 4750 replicates that yielded the smallest Kolmogorov-Smirnov (K-S) statistic [Conover, 1999] when compared to the predicted CAD (solid black line in Figure 6). Thus, the gray confidence band around the predicted CAD of Figure 6 represents the statistical uncertainty of the observed CADs. Please note that we just use the K-S statistic and not the K-S test. The K-S statistic is the largest vertical distance between two CDFs. Based on this statistic, Kolmogorov [1933] and Smirnov [1939, 1948] devised a test to decide whether or not sampling statistics alone could be responsible for the difference between two distributions. This test does not account for the measurement uncertainties of the data.



**Figure 7.** Quantile-quantile (Q-Q) plot of expected versus observed AFT ages. Young ages are overrepresented in sample C (single sample of sand), indicating that it was derived from low elevations. The CADs of the composite sample D are closer to the predicted distribution, indicating that over longer time scales, sediments are derived from the entire drainage, albeit with greater contributions from lower elevations than from further away.

However, this is irrelevant to the extent that only the K-S statistic, and not the actual K-S test is used for calculating the confidence band of Figure 6.

[32] The studies of Brewer et al. [2003] and Ruhl and Hodges [2005] were located in a very remote and challenging Himalayan field area, with relatively poorly known lithology and structural geology. Because these conditions made it very hard to assess the potential impact of nonuniform lithology and differential exhumation, these factors were not discussed in much detail. Ruhl and Hodges list non-uniform lithology and differential uplift under their assumption 2. They argue that if the observed CAD matches the hypsometry, this can be seen as evidence for the validity of these assumptions. In contrast with these previous studies, the White Mountains in general, and the Marble Creek drainage in particular provide an excellent testing ground for the CAD method, because both structure and lithology are simple. Nearly the entire catchment is underlain by a single pluton, the Pelissier Flats monzo-granite, which is bounded to the west by a single normal fault, but remains unaffected by faulting elsewhere. One potentially important lithological inhomogeneity are the mylonites of the Cretaceous White Mountain shear zone [Stockli et al., 2003]. As a first-order test of relatively uniform composition, note that all the Pelissier Flats samples of Stockli et al. [2000, 2003] yielded abundant apatite. A small but significant part of the canyon is Paleozoic marble [Crowder et al., 1972; Figure 2] that contains no apatite and will not contribute to the CAD. The dashed lines on Figure 6 were calculated assuming a uniform lithology with uniform apatite concentration. The two solid lines on Figure 6 show the equivalent predicted CADs excluding the marble outcrop; their difference illustrates the sensitivity of the CAD

to lithological inhomogeneity, which appears to be only moderately important.

# **3.2.** Using the CAD for Quantitative Geomorphology by Comparing Observed With Predicted CADs

[33] The gray circles on Figure 6 show the observed CAD of sample C (sand collected at the apex of the alluvial fan). The difference with the predicted CAD is immediately apparent. A useful tool for comparing two (cumulative) distributions is the quantile-quantile (Q-Q) plot [*Rice*, 1995, p. 353]. In a O-O plot, the quantiles of one distribution are plotted against those of another. Two distributions are equal if and only if they plot on the 1:1-line. This is clearly not the case for the CAD of sample C (gray circles on Figure 7). Sample C consists of very young ages between 6 and 19 Ma indicating that it was derived from very low elevations. This very localized provenance of sample C suggests that sediments in the presently active Marble Creek are derived from a single rockfall event localized very close to the mouth of the Marble Creek drainage, at an elevation of at most 500 m above the sample location (Figures 1 and 2).

[34] Thus far, we have studied clasts A and B and a single sand sample C. The next logical study is a composite of the entire alluvial fan, in an attempt to get a more integrated view of the entire drainage basin. 47 samples were collected from all over the alluvial fan (sample D: circles on Figure 2). These samples can be jointly considered, because the time span covered by fan surfaces in debris flow dominated alluvial fans of the Owens Valley is relatively short (<100 ka; Dühnforth et al. [2007]). To estimate the possible importance of grain-size induced bias, these samples were divided into a coarse (5 cm > clasts > 7.925 mm) and a fine (2.794 mm > clasts > 0.595 mm) fraction. Then, the samples from each of the two groups were mixed and dated with the AFT method. The resulting CADs are shown as white squares and black circles on Figure 6. Most apatites in the composite sample are older than sample C. The coarse fraction appears to be slightly younger than the fine fraction, but the difference is not statistically significant (compare the distance between the two CADs with the width of the gray confidence band in Figure 6), and we may conclude that grain-size effects are not very important. Just as we did for sample C, we compare the observed and predicted CADs for sample D by plotting them on a Q-Q plot (Figure 7). This analysis indicates that the composite sample was derived from the entire drainage. Most of the sediment was derived from low elevations, with smaller contributions from further awav.

[35]  $\sim$ 5% of the detrital grains in sample D have a zero AFT age whereas other apatites appear to be well over 100 Ma old, apparently contradicting the 10–55 Ma age range predicted by the PAZ curve of *Stockli et al.* [2000]. At first glance, this observation seems to suggest that some apatites are derived from outside the Marble Creek catchment. There are at least two possible sources for such "contamination": (1) the catchment is down wind from the Long Valley caldera, and the area was likely covered by a thick layer of Bishop volcanic ash; and (2) eolian processes in the arid Owens Valley might contaminate the Marble Creek alluvial fan with modern dust. The first possibility can be ruled out because the relatively coarse grain-size of sample D allowed verification of its granite and marble composition. Virtually

no tuff was found. The coarse grain-size of sample D also drastically reduces the probability of modern eolian contamination. Alternatively, the "anomalous" AFT ages can be much more easily explained by the counting statistics discussed in section 2.

#### **3.3.** Suggestions for Future Improvements

[36] The CAD method would gain considerable power if the AFT data were complemented by (U-Th)/He measurements as was done by Stock et al. [2006] for two catchments in the Sierra Nevada. Whereas the AFT CAD serves as a proxy for the PAZ curve, the (U-Th)/He CAD would be a proxy for the Partial Retention Zone (PRZ) curve. Because (U-Th)/He ages from the northern White Mountains have already been measured [Stockli et al., 2000], this would be relatively easy to do. Measurement uncertainties of singlegrain (U-Th)/He measurements are approximately normally distributed, and typically much smaller than single grain AFT measurement uncertainties. Unfortunately, this is only true for inclusion-free apatites. The vast majority of igneous apatites contain abundant  $\alpha$ -emitting mineral inclusions such as zircon and monazite, and the Pelissier Flats apatites are no exception to this. In basement studies, inclusion-free apatites are carefully selected under a binocular microscope. Not only would doing this for  $\sim 100$  detrital grains be very time-consuming but it would also create potentially biased samples. Therefore detrital (U-Th)/He studies should also consider inclusion-bearing grains [Vermeesch et al., 2007].

[37] Another approach to obtain more and better information from the AFT data is by artificially increasing the number of confined fission tracks through heavy-ion irradiation or exposure to <sup>252</sup>Cf [e.g., Ohira et al., 1994]. Like the AFT ages, fission track lengths show a dependence on paleodepth (and thus elevation). At low and high paleodepths well above or below the paleo-PAZ, fission tracks are long, whereas in the PAZ, short tracks also exist. Each AFT age on Figure 1a corresponds to a characteristic distribution of horizontally confined fission track (HCFT) lengths. Heavy ion irradiation or bombardment by <sup>252</sup>Cf fission fragments provides pathways through which the etching acid can reach more HCFTs, up to a point where there is more than one HCFT per apatite grain, even for samples with low numbers of spontaneous fission tracks [Ohira et al., 1994]. If the HCFT lengths and AFT ages of the same grains are measured, the provenance paleodepth distribution can be determined more reliably than by only using the AFT ages. The Marble Creek catchment would be the perfect test case for this technique, because the HCFTlength distribution of the basement is known [Stockli et al., 2000, 2003].

### 4. Conclusions

[38] Apparent ages of low-temperature thermochronometers generally decrease with depth below the surface. When basement terranes are uplifted, this variation produces an age-elevation dependence. Therefore it may be possible to recover the provenance elevation of the erosional products of exhumed fault blocks. This paper introduced the Cumulative Age Distribution as a tool for comparing observed detrital age distributions with hypsometric predictions. The CAD is the cumulative density function of the measured ages. Arguably the most important advantage of the CAD over alternative approaches is that it visualizes the detrital sample without the need for data smoothing. (Unequal) measurement uncertainties are incorporated in a hypsometrically predicted CAD by numerically simulating the sampling process. The statistical variability caused by the combined effects of limited sample size and analytical uncertainty can be estimated and visualized with a bootstrapped confidence interval of the predicted CAD.

[39] If (1) apatite concentration is uniform across the entire drainage basin, (2) measurement uncertainties are small, and (3) erosion is uniform across the entire drainage basin, then a hypsometrically weighted CAD of detrital AFT data has the same shape as the PAZ curve of the basement. Under the aforementioned assumptions, it would be possible to use the CAD as a tool for paleo-relief reconstruction, by studying sequential CADs through time, where the modern CAD is used to calibrate the older ones (i.e., convert cumulative percentages to meters), thus taking the approach suggested by Stock and Montgomery [1996] one step further. Unfortunately, very few if any field areas fulfill all three requirements. If assumption (3) is not valid, the method is still useful, because testing assumption (3) yields useful quantitative geomorphological information. The CADs of the White Mountains reveal that sediments in the currently active Marble Creek are derived from a single point source, but composite samples of the entire alluvial fan are derived from the whole catchment, with the largest contributions from the base of the range and lower contributions from higher up the drainage.

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P. Vermeesch, Institute of Isotope Geology and Mineral Resources, ETH Zürich, Clausiusstrasse 25, NW C85, CH-8092 Zürich, Switzerland. (pieter.vermeesch@erdw.ethz.ch)